

# Synthesis, Characterization and Application by HVOF of a WCCoCr/NiCr Nanocomposite as Protective Coating Against Erosive Wear

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## Keywords:

WCCoCr  
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Nanocomposite  
High energy milling  
HVOF  
Erosive wear

## ABSTRACT

The scope of this work is to synthesize and characterize a WCCoCr/NiCr nanocomposite evaluating its application as protective coating against erosive wear when applied by High Velocity Oxygen Fuel (HVOF). The composite was formed by carbide of tungsten-cobalt-chrome (WCCoCr) processed by high energy milling and a metallic matrix of nickel-chrome (NiCr). The milled material was added to the NiCr in the fraction of 5%wt. The powders were investigated by X-ray diffraction and scanning electron microscopy, analysing particle size distribution and surface area. The protective layers were deposited by HVOF and evaluated for their microhardness, microstructure, porosity, and erosive wear. Their microstructure showed lamellar character, with a low level of oxides and porosity between 0.5 % and 1 %. The coating formed by NiCr and WCCoCr milled for 3 hours presented microhardness of 635 HV and erosion rates 50 % smaller than the commercial coating.

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## 1. INTRODUCTION

Erosive wear affects numerous industries nowadays, such as oil and gas [1-2], power generation, mining, ground motion, metalworking, aerospace or automotive. Components failures may result in significant financial loss and environmental troubles [3]. Thus, many studies dealing with technical solutions, materials and wear-resistant coatings have been carried out in the recent years in order to increase components service life [4-9]. In the oil industry, in particular, the erosive

wear is mainly caused by the presence of solid particles such as sand. The continuous impact of sand particles inside pipelines, valves and other equipment causes extensive damages. The worst-case scenario generally occurs where there is a co-presence of both erosion and oxidation, especially in the cases of higher temperatures. The corrosive degradation is accelerated by the erosive mechanism attributed to the sand impingement, resulting in a synergistic effect known as 'erosion-corrosion' [10]. Tungsten-cobalt carbide (WCCo) and nickel-chrome carbide-based (NiCr) coatings are

widely used in the way to improve the wear resistance [11-17]. These ceramic-metallic materials (cermets) consist of ceramic particles embedded in a metal matrix. The particles in ceramic offer a high erosion resistance. The metallic matrix makes the coating more ductile than a pure ceramic coating [18]. NiCr systems stand out since they can be utilized at higher temperature under wear and corrosion [7].

Also, they are considered to be an excellent replacement to electrolytic hard chrome in the realisation of thick and wear-resistant coatings [19,20].

WCCo and NiCr cermets can be in general deposited by thermal spray processes such as detonation spray, and high-velocity oxygen fuel spray (HVOF). The high particle velocity and the low flame temperatures by HVOF method produce coatings with the following properties: high densification, strong adhesion between coating and substrate, low residual stress, low porosity (typically <1 %) and low chemical decomposition of WC particles [7,21,22].

Many studies about WCCo coatings use conventional commercial spray powders material [14,23-25]. The utilization of nanostructured materials may increase the performance of these coatings. The physical and mechanical properties of these materials are better because of the reduced grain size and of the high volumetric fraction of atoms in the grain boundary [26]. Refinement of grain sizes down to nanometer range can be achieved by mechanical alloying (MA) [27]. Nanostructured powders produced by MA possess physical and mechanical properties different from those of materials prepared by conventional techniques [28]. MA is a high-energy ball milling technique used to produce a variety of materials, such as borides, carbides, nitrides, oxides and nanocomposites [29-33]. Many studies have been conducted about WCCo nanocomposites obtained by high energy ball milling [34-40].

This research investigates in details the process of synthesis of a WCCoCr/NiCr nanocomposite coatings, permitted by high energy milling technique, and evaluates the effects of its application by high velocity oxygen fuel (HVOF) spray technology in terms of protection against erosive wear.

## 2. MATERIAL AND METHODS

### 2.1 Materials

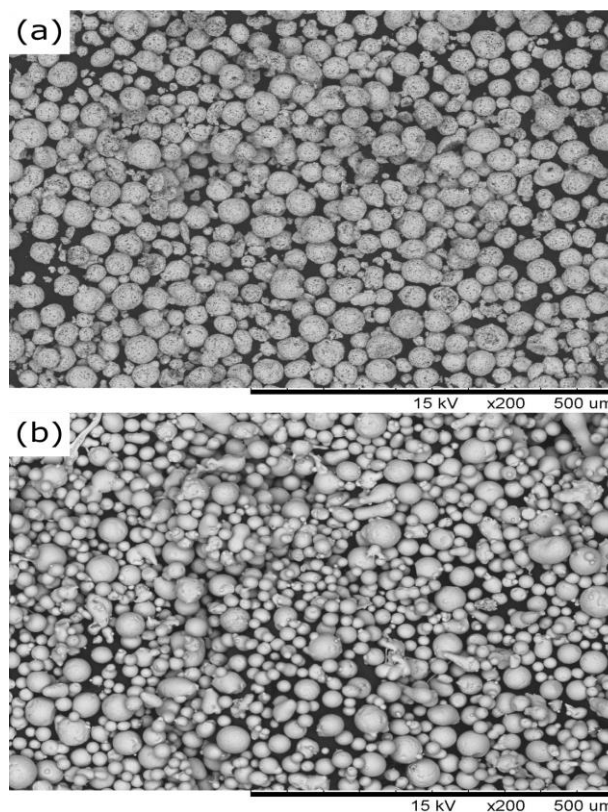
The carbide of tungsten-cobalt-chrome (WCCoCr) and nickel-chrome (NiCr) employed were produced by Sulzer Metco (Woka 3652 and Diamalloy 2001, respectively). Tables 1 and 2 show the chemical composition of the starting powders.

**Table 1.** Chemical composition of WCCoCr commercial powder.

Element	Composition (%)
W	Balance
Co	8.5 - 11.5
Cr	3.4 - 4.6
C	4.8 - 5.6
Fe	0.2

**Table 2.** Chemical composition of NiCr commercial powder.

Element	Composition (%)
Ni	Balance
Cr	17
B	3.5
Si	4
C	1
Fe	4



**Fig. 1.** (a) SEM images of WCCoCr and (b) NiCr particles as-received.

Figures 1a-1b show the morphology of WCCoCr and NiCr as-received, respectively. Both materials display a spheroidal morphology, which is characteristic of the production process employed. WCCoCr was agglomerated and sintered, while the NiCr was gas-atomized.

### 2.2 Synthesis of WCCoCr/NiCr nanocomposites

The high energy ball milling of WCCoCr was carried out at room temperature, using a planetary ball mill (Pulverisette 6, Fritsch). A tempered steel grinding bowl and AISI 52100 steel balls, with 10 mm in diameter, were used. The milling was performed in ethanol medium, using a ball-to-powder ratio (BPR) of 1:1, a milling speed of 450 rpm and three milling times (3, 6 and 12 hours). WCCoCr was added to NiCr in the amount of 5 %. The mixture was agglomerated and treated thermally (heating rate: 100 °C/min; dwell 1: 3h at 350 °C; dwell 2: 6h at 850 °C).

### 2.3 Nanocomposites characterization

Powders obtained by high energy ball milling and the alloys formed by the mixture of WCCoCr and NiCr were characterized by X-ray diffraction (XRD), particle size analysis, surface area, and scanning electron microscopy (SEM).

**Table 3.** XRD analysis parameters.

Parameter	Phase analysis	Crystallite size
$\Delta 2\theta$	25° - 105°	34° - 38°
Step	0.05	0.04
Time per step (s)	1	4
Cracks	½	¼

The crystalline phases and crystallite sizes were determined using X-ray powder diffraction (Phillips diffractometer, X'Pert MPD model). The diffractometer has a graphite monochromator, Cu-K $\alpha$  radiation ( $\lambda = 1.5406$ ), and a fixed anode operated at 40 kV and 40 mA. Table 3 shows the selected parameters for the phase analysis and determination of the crystallite size. Crystallite size was calculated by measuring the Bragg peak width at half maximum intensity and using the Scherrer's equation (1):

$$\beta = \frac{0.9 \cdot \lambda}{D \cdot \cos \theta} \quad (1)$$

where:

D is the crystallite size,

$\beta$  is the pure broadening of the diffraction peak measured at half maximum intensity,  $\lambda$  is the wavelength of the X-ray radiation used,  $\theta$  is the Bragg angle [41].

The average grain diameter was measured with a CILAS 1180 particle size analyser (CILAS). The surface area was determined by the Branauer, Emmett and Teller method [42], using an Autosorb Quantachrome (model NOVA 1000) apparatus. The microstructure of the milled WC-Co powders was observed by a scanning electron microscope (SEM, Hitachi-TM 3000).

### 2.4 Thermal spray coating deposition

The coatings were deposited using a TAFE JP5000 HVOF spray system (PRAXAIR SURFACE TECHNOLOGIES Inc) with process parameters listed in Table 4. A substrate of AISI 310 stainless steel with cylindrical format (30 mm X 6 mm) was used. The substrates were grit-blasted with Al<sub>2</sub>O<sub>3</sub> before spraying to provide a roughened surface. No thermal treatment was performed on the substrates.

**Table 4.** HVOF process parameters.

Parameters	Values
Kerosene flow rate (l/min)	0.385
Oxygen flow rate (m <sup>3</sup> /h)	58.2
Feed rate (m <sup>3</sup> /h)	0.3
Spray distance (mm)	300 mm

### 2.5 Coating characterization

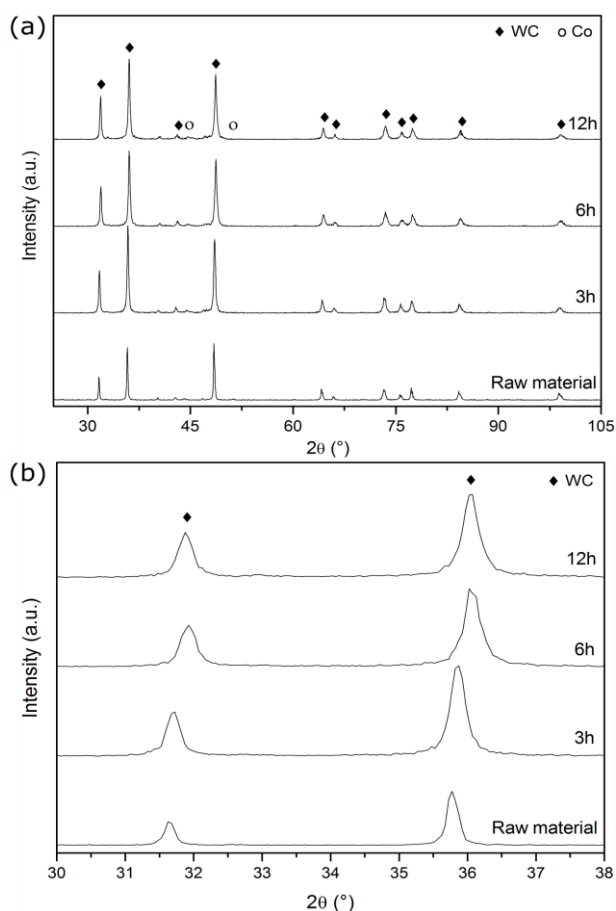
Vickers microhardness tests were performed using a Buehler Micromet 2000 with a load of 3 N. Indents were placed in matrix and carbides areas. Microstructural characterization of the coatings was carried out by an Olympus BXS1M microscope. Porosity analysis was done using image analysis software (Image J), after ASTM E2109-01 [43].

The equipment used in erosive wear tests is based on [44]. The details of the experimental set-up are presented in [45-46]. Electromelted alumina was used as erodent. Tests were performed at room temperature, with incidence angles of 30° and 90°. Erosion rate of the coatings were measured by weight loss.

### 3. RESULTS AND DISCUSSION

#### 3.1 WCCnCr processed by high energy ball milling

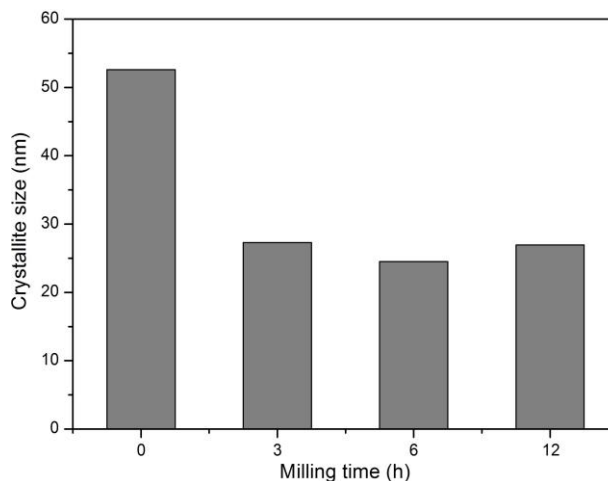
Figure 2a shows the XRD diffractograms of the raw material and the ball-milled powders. The presence of the WC (JCPDS 00-051-0939) and Co (JCPDS 00-015-0806) phases can be identified. Figure 2b shows the two first diffraction peaks shown in Fig. 2a in detail. After ball milling, the diffraction peaks broaden, as a result of the reduction in crystallite size and the enhancement of its internal strain [27,47]. This behaviour was observed by [39] for short milling times, and by [38,48-50] for long milling times.



**Fig. 2.** (a) X-ray patterns of WCCoCr particles as-received and after ball milling, (b) Detailed X-ray patterns of the first two diffraction peaks of WCCoCr particles as-received and after ball milling.

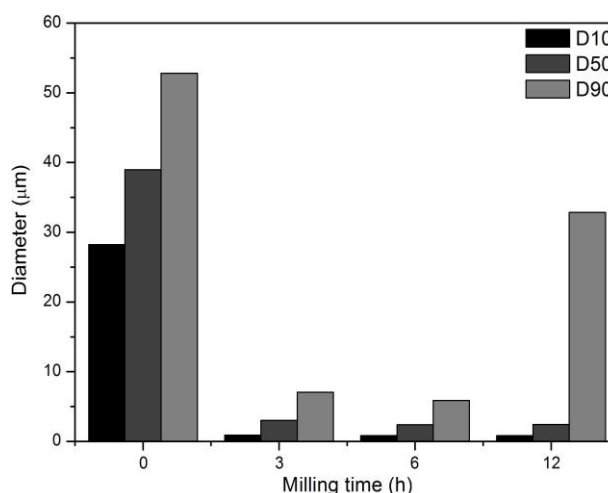
The crystallite size development as function of the milling time is shown in Fig. 3. An important reduction of crystallite size for the first hours of milling can be observed. The crystallite size decreases with the enhancement of the milling time, and achieves a relatively constant value.

Crystallite sizes are smaller than 30 nm. Enayati [38] and Xueming [48] obtained crystallite sizes of nearly 10 nm. This difference may be explained by the higher BPR's (10:1 and 30:1, respectively) used by these authors. On the other hand, [40] obtained a large crystallite size (45 nm) using a milling time of 25 hours and a milling speed of 130 rpm.



**Fig. 3.** Crystallite size of WCCoCr as function of milling time.

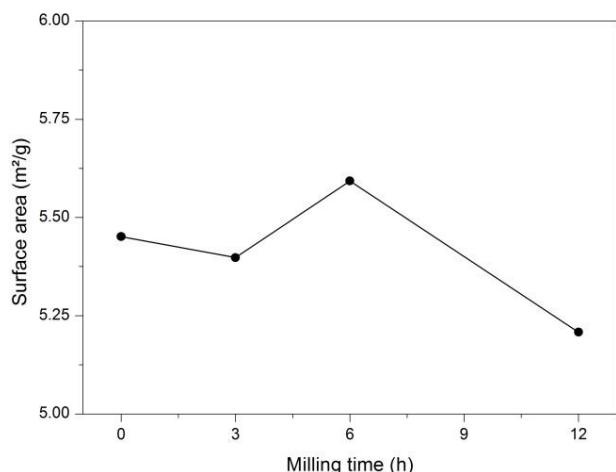
Figure 4 displays the D10, D50 and D90 variation as function of the milling time. A significant reduction of the particle size after 3 and 6 h of milling can be observed, due to fracture of the coarse fraction. D90 increases for the milling time of 12 h, probably due to the overlap and the cold welding of small fragments [27].



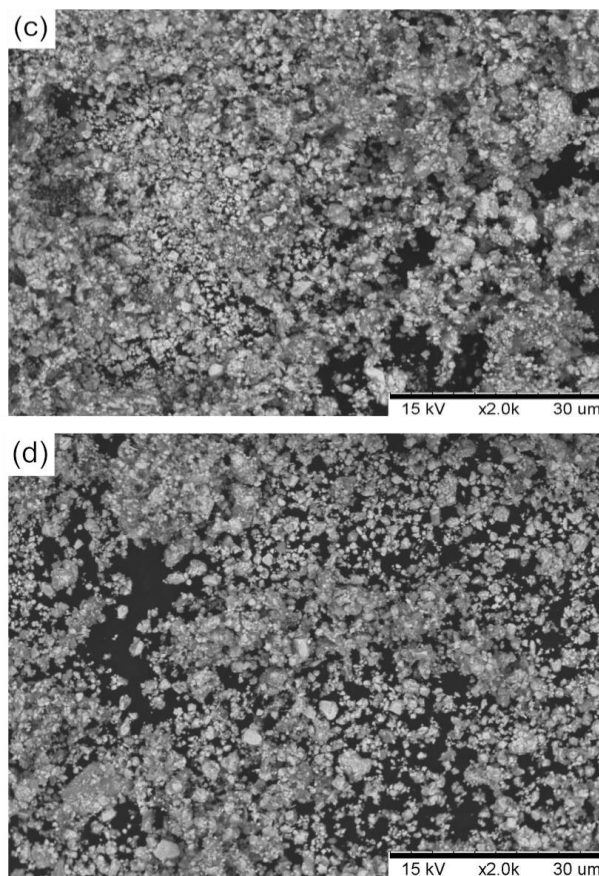
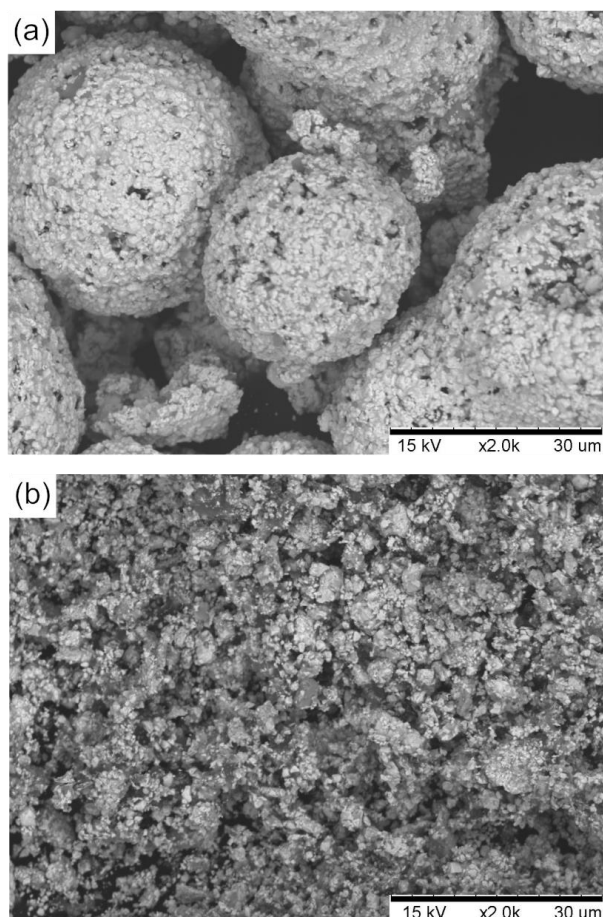
**Fig. 4.** D10, D50 and D90 of WCCoCr as function of milling time.

The surface areas of the WCCoCr processed as function of the milling time are shown in Fig. 5. The highest surface area was observed for the

sample milled for 6 h, which has the smallest crystallite size (Fig. 3). All samples had a small change in the surface area compared to the material without milling (with  $SA=5.451\text{m}^2/\text{g}$ ). This behaviour was observed by [37] during preparation of a WC-12Co alloy by mixing WC with Co in a planetary mill. The surface area of the material obtained by the researchers increased with the milling time. After a milling time of 25 h, the surface area achieved the value of  $4.687\text{m}^2/\text{g}$ .



**Fig. 5.** Surface area of WCCoCr particles as function of milling time.

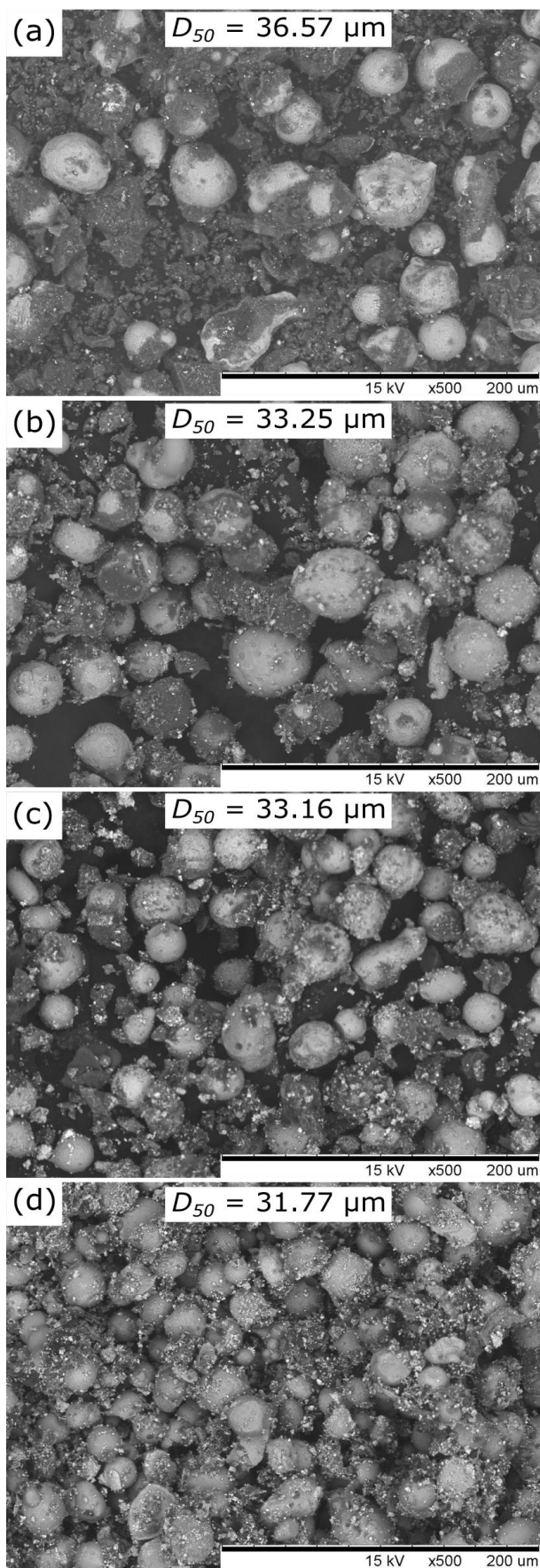


**Fig. 6.** SEM images of WCCoCr as raw material (a), and as milled powder by 3 h (b), 6 h (c) and 12 h (d).

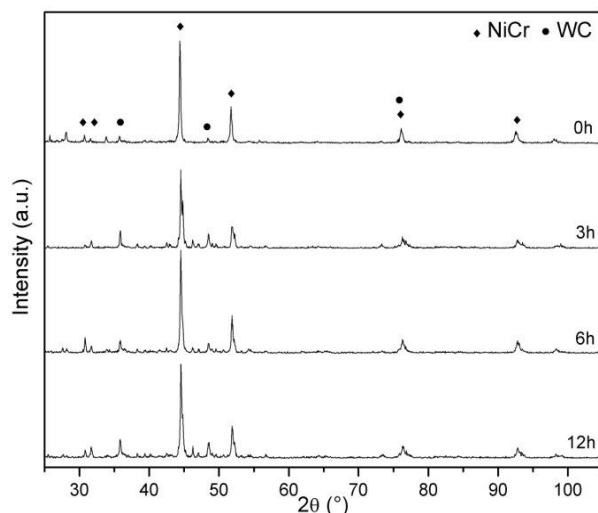
Commercial material particles (Fig. 6a) were nearly spherical, typical of the production process used (agglomeration and sintering). Figures 6b-6d show the material after 3, 6 and 12 h of milling, respectively. After ball milling, the particles were fragmented into fine powder. The WCCoCr particles lost their starting morphology and had their size significantly reduced in the first hours of milling. Significant modifications in the powders morphology were also detected by [33,38,51]. WCCoCr milled for 6 h (Fig. 6c) showed particles smaller than the sample milled for 12 h (Fig. 6d). This is also in accordance with the average value measured for the grain diameter.

### 3.2 WCCoCr-NiCr nanocomposites

Figure 7 shows the SEM images and the particle median size (D50) of the alloys formed by the mixture of 5 % of WCCoCr and NiCr. All samples presented spherical and larger particles of NiCr, and smaller particles of WCCoCr. The samples with milled WCCoCr presented particles smaller than the samples with raw material. All samples showed particle median size appropriate for utilisation in HVOF spray systems.



**Fig. 7.** SEM images of the alloys formed by the mixture of 5 % of WCCoCr and NiCr. WCCoCr as raw material (a), and as milled powder by 3 h (b), 6 h (c) and 12 h (d).

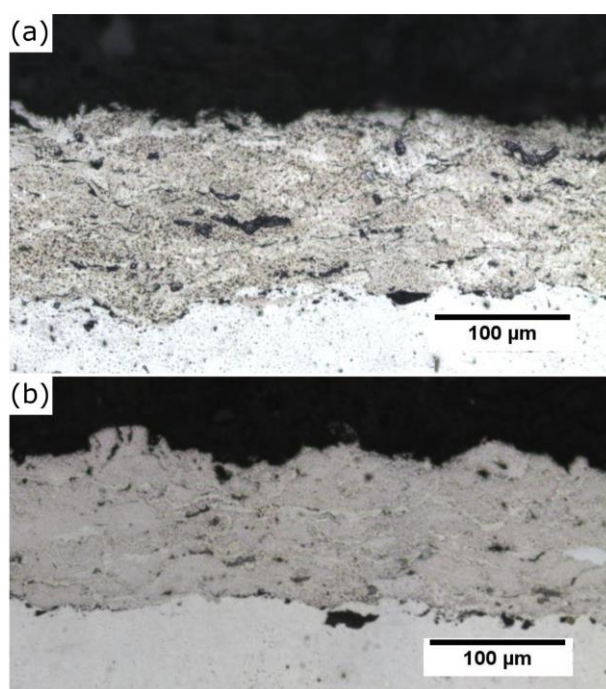


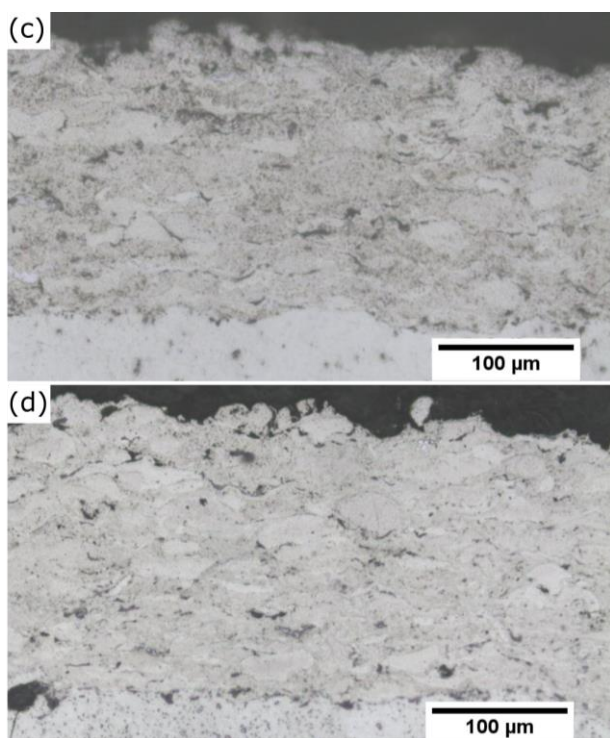
**Figure 8:** X-ray patterns of the alloys formed by the mixture of WCCoCr and NiCr.

Figure 8 shows the XRD diffractograms of the alloys formed by the mixture of 5 % of WCCoCr and NiCr. The presence of the tungsten carbide (WC) and nickel-chrome (Cr<sub>1.12</sub>Ni<sub>2.88</sub>) phases can be identified.

### 3.3 WCCoCr-NiCr Coating

Figure 9 shows the microstructures of the layers obtained by thermal spray of the WCCoCr-NiCr alloys. The microstructures presented low quantity of oxides. The coating obtained with as-received WCCoCr (Fig. 9a) did not show lamellas. Other coatings' microstructure (Figs. 9b-9d) showed a more evident lamellar character.





**Fig. 9.** Coating microstructure of WCCoCr-NiCr alloy with 5% of WCCoCr raw material (a) and milled by 3 h (b), 6 h (c) and 12 h (d).

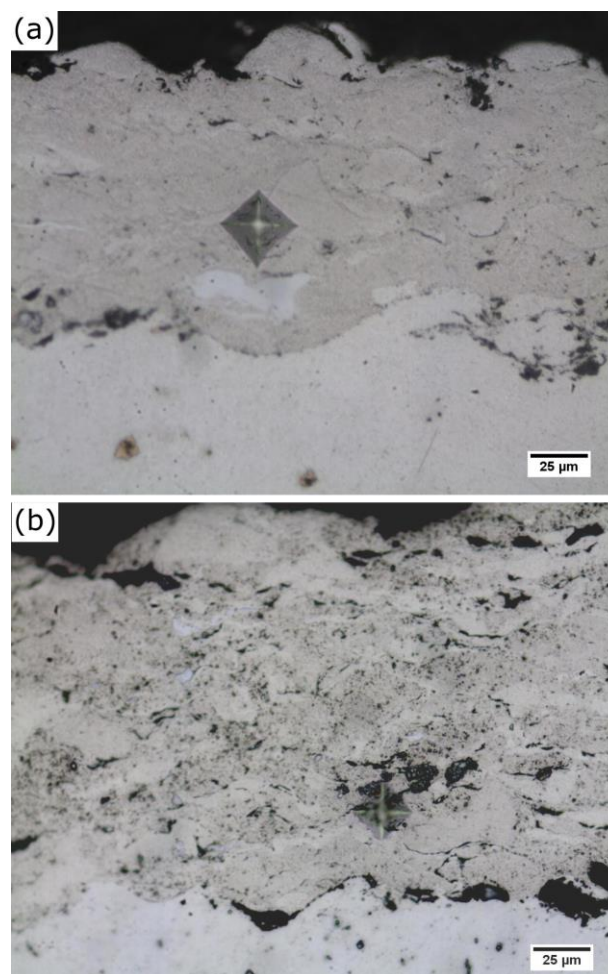
After analysis of three samples of each coating, the average porosity was quantified between 0.5 and 1 %, according to [43]. Berger et al. [52] obtained porosity between 0.7 and 1.8 % for a WC-NiCr. Thakur et al. [13] compared two WC-Co-Cr coatings: the first with carbide size between 200 and 500 nm, and the second with 100 nm. The porosities obtained were 0.75 % and 0.57 %, respectively.

**Table 5.** Microhardness coatings.

Coating	Microhardness Matrix (HV)	Microhardness Carbides (HV)
raw material	424	876
3 h	404	635
6 h	406	823
12 h	406	598

Microhardness tests were implemented in the coatings matrix and in the areas with probable presence of carbides. Table 5 shows microhardness values for both areas. The identification of areas with higher microhardness, possibly containing carbides, was more evident for the coatings with 5 % of WCCoCr raw material and 5 % of WCCoCr milled for 6 hours. The carbides were dispersed in a NiCr matrix of the coatings 5 % of WCCoCr milled for 3 h and 12 h. Figure 10a shows an indentation in the matrix

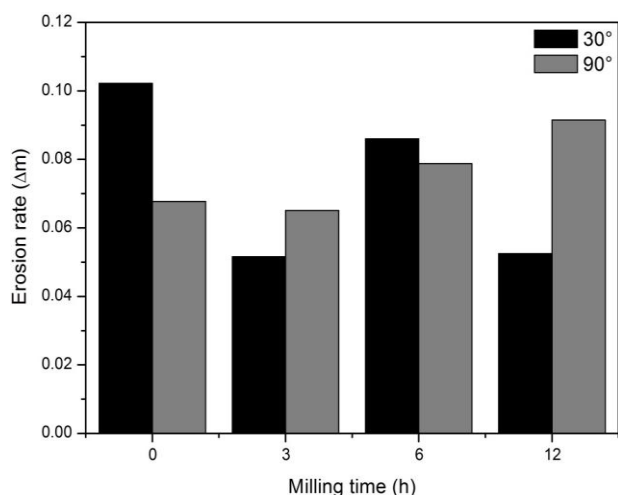
area for the coating 5 % of WCCoCr 3 h. The average microhardness (404 HV) indicates that this area is more ductile. Figure 10b shows an indentation in the carbides area for the coating 5 % of WCCoCr 6 h. This coating presented microhardness of 823 HV. Murthy and Venkataraman [19] obtained a similar result (836 ±30 HV) for a WCCoCr coating. Berger et al. [52] reported a microhardness of 1012 ±90 HV for a WC-NiCr coating.



**Fig. 10.** (a) Indentation in the matrix area for the coating of WCCoCr-NiCr with 5% of WCCoCr milled for 3 h. (b) Indentation in the carbide area for the WCCoCr-NiCr with 5% of WCCoCr milled for 6 h.

Figure 11 shows the erosion rate, in weight loss, for the WCCoCr-NiCr coatings. In the tests performed with an attack angle of 30°, the coatings obtained with nanostructured WCCoCr had smaller erosive wear than the coating obtained with WCCoCr raw material. The coatings formed by WCCoCr milled for 3 and 12 h showed similar performance and erosion rate 50 % smaller than the commercial coating. In the tests performed with an attack angle of 90°,

the erosion rate increased for milling times higher than 6 hours.



**Fig. 11.** Erosion rate of the wccocr-niCr coating.

The protection obtained with WCCoCr milled for 3 h showed erosion rate lower than the raw material. The coatings 5 % WCCoCr commercial and 6 h presented higher erosive wear in 30° than in 90°, indicating behavior of ductile material. On the other hand, the coatings 5 % WCCoCr 3 and 12 h showed higher erosive wear in 90°, indicating a brittle behavior [53-54].

#### 4. CONCLUSIONS

According to the results presented, it can be concluded that:

- High energy ball milling was effective to refine the microstructure of WCCoCr powders to a nanometer scale size. The crystallite size was smaller than 30 nm after 3 hours of milling. The WCCoCr particles lost their starting morphology and had their size significantly reduced in the first hours of milling. For longer milling times, occurred the overlap and the cold welding of small fragments, increasing the mean diameter.
- The coatings showed lamellar character, with low level of oxides and porosity inside the range of 0.5 % and 1 %.
- The coatings obtained with 5 % of WCCoCr milled for 3 and 12 h presented carbides more dispersed in the NiCr matrix. On the other side, the carbides were observed in concentrated areas in the coatings with 5 % of WCCoCr raw material and milled for 6 h.

- The erosive wear was higher for the attack angle of 30° for the coatings with 5 % of WCCoCr raw material and milled for 6 h. For this attack angle, the erosive wear is higher for the materials that show ductile behaviour.
- The coating with 5 % of WCCoCr milled for 3 h presented microhardness of 635 HV with an erosion rate of 50 %, smaller than the commercial coating for the attack angle of 30°.

#### Acknowledgement

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